Using Generalised Polynomial Chaos to Examine Various Parameters in a Half-ellipsoidal Ventricular Model of Partial Thickness Ischaemia

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Abstract

Elevation and depression in the ST segment of the electrocardiogram is commonly used as part of a diagnosis of myocardial ischaemia, although there is not yet a clear correlation between these observations and partial thickness ischaemia. In this work, we use a half-ellipsoid bidomain model of subendocardial ischaemia in a ventricle to study the effect of changes in model parameters on ST segment epicardial potential distributions (EPDs). We use generalised polynomial chaos techniques to produce mean EPDs, where the six bidomain conductivity values are varied, as well as blood conductivity and fibre rotation, for a number of different representations of the ischaemic region.

We find that, as the thickness of the ischaemic region (i.e. the ischaemic depth) increases, the character of the mean EPD first changes from a single minimum approximately above the ischaemic region, to a maximum over the ischaemic region, with the minimum moving to a border of the ischaemic region. Next a second minimum develops, in addition to the previous maximum and minimum. In contrast, the strength of the maximum and the minima is only affected in a minor way by changes in the width of the ischaemic border and the position of the ischaemic region, provided it is not near the apex or base of the ventricle. When the size of the ischaemic region is increased, the magnitudes of both the maximum and the minima increase, but their character does not change.

In summary, the qualitative progression of the mean EPD with increasing ischaemic depth, from single minimum through to a maximum surrounded by two minima, is the same, regardless of the size and position of the ischaemic region.

1. Introduction

Simulation studies are an important tool for studying the effects of myocardial ischaemia on the electrocardiogram, and, in particular, the effects of subendocardial ischaemia, since it is less well-understood than transmural ischaemia. If these studies are to be clinically useful, it is important that modellers are able to quantify, in some fashion, the effects of the various modelling assumptions and parameter choices they make in their models.

Some previous work in this area has used simplified model geometries for the left ventricle (e.g. slabs, cylinders, half-ellipsoids [1]), while other work uses more realistic geometries [2, 3]. Another study [4] has looked at the effect of the shape of the ischaemic region on the epicardial potential distributions (EPDs) that are produced.

The majority of recent work represents the cardiac tissue as consisting of interpenetrating bi-domains, intracellular (i) and extracellular (e). In these the current is assumed to flow in three mutually orthogonal directions, longitudinal (l), transverse (t) and normal (n), that is along, across and between the sheets of cardiac fibres, respectively. This leads to six bidomain conductivity parameters \( g_{pq} \) (where \( p = i, e \) and \( q = l, t, n \)) in the model, in addition to other parameters, such as the blood conductivity \( g_b \) and the angle (ROT) that represents the overall rotation of the sheets of cardiac fibres between the epicardium and the endocardium.

A recent study [5] has systematically quantified the effect of these parameters in a slab model and this work is part of a similar study in a more realistic half-ellipsoidal model. Here we analyse and compare mean EPDs, produced via polynomial chaos techniques, to gauge the effect of changes in the thickness, size and position of the ischaemic region, as well as in the representation of the transmembrane potential in the model (i.e. the ischaemic border), on the character of the EPD.

2. Methods

2.1. Half-ellipsoidal model

The left ventricle of the heart is modelled [1] using half of the ellipsoid represented by the equations

\[
x = a \cos \theta \cos \phi, \quad y = a \cos \theta \sin \phi, \quad z = c \sin \theta
\]  

(1)
with \(-\pi \leq \phi \leq \pi\) and \(0 \leq \theta \leq \pi/2\). For the endocardial surface, which is in contact with the blood volume, we set \(a = 2\) and \(c = 4\), and for the epicardial surface \(a = 3\) and \(c = 5\), giving a tissue thickness of 1 cm throughout the model (Figure 1). The ischaemic region is represented by a ‘rectangular’ patch of tissue \((-15^\circ \leq \phi \leq 15^\circ, 50^\circ \leq \theta \leq 70^\circ\) ), which varies in depth, depending on the degree of ischaemia (ISC).

We solve the passive bidomain equation [6] for the extracellular potential \(\phi_e\)

\[
\nabla \cdot (M_e + M_c) \nabla \phi_e = -\nabla \cdot M_i \nabla \phi_m \tag{2}
\]

on a mesh constructed on the above geometry, using a technique [1] based on the finite volume method. The conductivity tensors in the intracellular and extracellular spaces, \(M_p(p = i, e)\), respectively, are of the form \(M_p = AG_pA^T(p = i, e)\), where the diagonal matrix \(G_p\) contains the bidomain conductivity values \((g_{pq}, p = i, e, q = l, t, n)\) and \(A\) is a rotation matrix which maps the local fibre direction into the global coordinate system. We offset the cardiac fibres by \(-45^\circ\) on the epicardium and assume that they rotate linearly from the epicardium to the endocardium, through the angle ROT.

The transmembrane potential \(\phi_m\) during the ST segment is represented by [1, 6]

\[
\phi_m(r, \theta, \phi) = \Delta \phi_p \Psi(r_a - r) \Psi(\theta - \theta_0) \Psi(\phi) \tag{3}
\]

where \(\Delta \phi_p\) is the difference in plateau potentials between the normal and ischaemic tissue, and \((r_a, \theta_0)\) is the position of the centre of the ischaemic region on the endocardial surface. Here

\[
\Psi(t) = \begin{cases} 
1 - \exp(-a_t/\lambda_t) & |t| \leq a_t \\
1 - \exp(-a_t/\lambda_t) \sinh(a_t/\lambda_t) & |t| > a_t
\end{cases}
\tag{4}
\]

where \(a_t\) is the half-width of the ischaemic region for the \(i = r, \theta, \phi\) directions. We let \(\Delta \phi_p = -30\) mV [1, 7], and then initially set \(\lambda_t = 0.01\) \(\forall t\), to give a narrow border zone between the normal and ischaemic tissue.

We use the same boundary conditions as in previous work [1]; that is, we assume no current flux at the boundary of the intra- and extracellular domains at the air-tissue interfaces and at the blood-air interface. We also assume continuity of potential and current in the extracellular space at the blood-tissue boundary. Finally, the extracellular potential is set to zero at the apex of the ventricle.

### Table 1. Data ranges for model inputs in this study. Units are degrees for fibre rotation (ROT) and mS/cm for conductivities.

<table>
<thead>
<tr>
<th>Parameter</th>
<th>Minimum</th>
<th>Mean</th>
<th>Maximum</th>
</tr>
</thead>
<tbody>
<tr>
<td>ROT</td>
<td>60</td>
<td>100</td>
<td>140</td>
</tr>
<tr>
<td>(g_b)</td>
<td>3.25</td>
<td>6.5</td>
<td>9.75</td>
</tr>
<tr>
<td>(g_l)</td>
<td>1.2</td>
<td>2.4</td>
<td>3.6</td>
</tr>
<tr>
<td>(g_t)</td>
<td>1.2</td>
<td>2.4</td>
<td>3.6</td>
</tr>
<tr>
<td>(g_{cl})</td>
<td>0.12</td>
<td>0.24</td>
<td>0.36</td>
</tr>
<tr>
<td>(g_m)</td>
<td>0.8</td>
<td>1.6</td>
<td>2.4</td>
</tr>
<tr>
<td>(g_{cn})</td>
<td>0.05</td>
<td>0.1</td>
<td>0.15</td>
</tr>
<tr>
<td>(g_{en})</td>
<td>0.5</td>
<td>1.0</td>
<td>1.5</td>
</tr>
</tbody>
</table>

#### 2.2. Polynomial Chaos

In this study we use generalised polynomial chaos as a way of considering the effect that uncertainty in the inputs, which are based on literature values [5], may have on the outputs of the model. For each of the various scenarios considered, we achieve this by allowing the eight inputs in Table 1 to vary uniformly across the ranges given using stochastic collocation [8], with collocation points from a Clenshaw-Curtis numerical integration scheme. Then Smolyak’s method [9] is used to reduce the size of the integration space. Since we have eight input values, using level 2 integration results in \(j = 145\) integration points \((\text{ROT}^{(j)}, g_b^{(j)}, g_l^{(j)}, g_t^{(j)}, g_{cl}^{(j)}, g_m^{(j)}, g_{cn}^{(j)}, g_{en}^{(j)}, p = i, e, q = l, t, n)\) and integration weights \(w_j\). If we denote \(\phi_e^{(j)}\) to be the EPD that results for each of these 145 sets of conductivities, the mean and standard deviation (std) of the EPD, respectively, are given by

\[
\overline{\phi_e} = \sum_{j=1}^{145} w_j \phi_e^{(j)}, \quad (\phi_e)_{\text{std}} = \left( \sum_{j=1}^{145} w_j (\phi_e^{(j)} - \overline{\phi_e})^2 \right)^{1/2}
\]

#### 3. Results and discussion

##### 3.1. Variation with Ischaemic Depth

Using polynomial chaos, we present a set of mean EPDs (Figure 2) for ischaemic depths from 10% to 90%. These polar plots show the ellipsoidal surface flattened into a circle, with the radius of each node scaled according to its \(\theta\)
We also investigate the effect of moving the ischaemic patch closer to and further from the apex of the ventricle by running sets of simulations for each value of ISC and varying the original range of \( \theta \in [50^\circ, 70^\circ] \) from \( \theta \in [10^\circ, 30^\circ] \) in \( 10^\circ \) increments up to \( \theta \in [70^\circ, 90^\circ] \), with scaling so that the size of the patch stays approximately the same. A sample set of the potentials for the usual features of the mean EPDs, for \( \theta \in [30^\circ, 50^\circ] \), is given in the left-hand columns of Table 3. A comparison of these with those in the lefthand column of Table 2, where \( \theta \in [50^\circ, 70^\circ] \), shows that the moving the ischaemic region to this new position again has a minor effect on the potentials and no effect on the character of the EPDs. This is also true for the other positions of the patch that were investigated, except in some cases where the patch is placed close to either the apex or the base of the ventricle.

### 3.4. Effect of a larger ischaemic region

The final scenario that we look at is that of a larger ischaemic patch, that is one with \(-20^\circ \leq \phi \leq 20^\circ, 50^\circ \leq \theta \leq 80^\circ\), rather than \(-15^\circ \leq \phi \leq 15^\circ, 50^\circ \leq \theta \leq 70^\circ\).
4. Conclusion

Our results are consistent with previous modelling studies in realistic hearts [2,3] that found that the EPD assumes a different character for low, medium and high thicknesses of the ischaemic region. However, systematic studies into the effect of different fibre rotation angles and also into the effect of varying the six bidomain conductivity values in realistic geometries have not yet been performed. This study paves the way for such studies by examining various modelling assumptions associated with the representation of the ischaemic region and showing that they have a minor effect on the character of the EPD.

References


A set of these plots for a range of ISC values is given in Figure 3 and the potentials corresponding to these EPD features are given in the right-hand set of columns in Table 3. When these are compared with the original values (left-hand columns of Table 2), we see that the magnitudes of all of min1, max and min2 are greater for the larger patch than for the smaller patch, for all values of ISC. However, it can also be seen that the plots in Figures 2 and 3 are qualitatively the same.