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Author

Beal, CD, Gardner, EA, Menzies, NW

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Process, performance and pollution potential: A review of septic tank – soil absorption systems

C. D. Beal^A, E. A. Gardner^B, N. W. Menzies^C,

^A School of Land & Food Sciences, University of Queensland; and Coastal CRC, Indooroopilly, Qld

^B Qld Department of Natural Resources, Mines & Energy; and Coastal CRC, Indooroopilly, Qld

^C School of Land & Food Sciences, University of Queensland, St Lucia, Qld 4073

Abstract

On-site wastewater treatment and dispersal systems (OWTS) are used in non-sewered populated areas in Australia to treat and dispose of household wastewater. The most common OWTS in Australia is the septic tank – soil absorption system (SAS) which relies on the soil to treat and disperse effluent. The mechanisms governing purification and hydraulic performance of a SAS are complex and have been shown to be highly influenced by the biological zone (biomat) which develops on the soil surface within the trench or bed. Studies suggest that removal mechanisms in the biomat zone, primarily adsorption and filtering, are important processes in the overall purification abilities of a SAS. There is growing concern that poorly functioning OWTS are impacting upon the environment. Though, to date, only a few investigations have been able to demonstrate pollution of waterways by on-site systems.

In this paper we review some key hydrological and biogeochemical mechanisms in SAS, and the processes leading to hydraulic failure. The nutrient and pathogen removal efficiencies in soil absorption systems are also reviewed, and a critical discussion of the evidence of failure and environmental and public health impacts arising from SAS operation is presented. Future research areas identified from the review include the interactions between hydraulic and treatment mechanisms, and the biomat and sub-biomat zone gas composition and its role in effluent treatment.

Additional keywords: biomat, LTAR, modelling, nutrients, pathogens, on-site systems, wastewater

Introduction

On-site wastewater treatment and dispersal systems (OWTS) are used in non-sewered populated areas in 20% of Australian households to treat and dispose of household wastewater. The most common OWTS in Australia is the septic tank – soil absorption system (SAS). Wastewater undergoes primary treatment in the septic tank via sedimentation and anaerobic digestion. Secondary treatment of the septic tank effluent occurs within the trenches or beds and surrounding soil (Figure 1). A SAS utilises the soil as the medium to treat and disperse effluent originating from the septic tank.

Fig 1.

Unlike alternative OWTS, the soil absorption system relies solely on the natural biogeochemical processes that occur in soil to assimilate various effluent pollutants. The advantage that this method has over other on-site systems is its relative simplicity, low cost and, if designed and constructed properly, treatment capability. The limitations of SAS relate to the inherent variability and heterogeneity of soil and soil biogeochemical processes. With aerated wastewater treatment systems (AWTS) the treatment processes (aeration, clarification, dispersion) can be directly controlled or regulated after system installation. Conversely, apart from septic tank inspections, the operation of a SAS is largely left to natural processes below the soil's surface. Consequently, appropriate design, construction, and maintenance, based on prior knowledge of the site and soil conditions, are crucial for the sustainable and successful operation of these systems. So it follows that an understanding of the processes that drive a SAS is essential for design and installation, and management in general. Nevertheless, success will not be achieved for every single system that has been designed, constructed and

maintained properly; the factors required to achieve that success are too numerous and too varied. However, substantial improvement to the current sustainability of SAS is more likely to occur as a result of informed and well-considered management.

The provenance of the OWTS regulatory criteria has placed an emphasis on reducing health risks associated with OWTS. The progression of the on-site treatment industry, in terms of the use of new technologies and the introduction of performance-based criteria, has been held back by its “public health heritage” (Otis 1991). This has resulted in often conservative and prescriptive criteria set by the responsible regulatory body. In the United States, SAS are the predominant on-site system with approximately 20 million systems in use. The USEPA response to Congress on the long-term viability of on-site systems, neatly summarises their point-of-view: “*Adequately managed decentralized wastewater treatment systems are a cost-effective and long-term option for meeting public health and water quality goals, particularly in less densely populated areas.*” (USEPA 1997). Despite this, SAS continue to have a mixed reputation in the industry and with the general public, and can be likened to “Dr Jekyll and Mr Hyde” in terms of its unpredictable and variable treatment efficiency and failure rates.

Some SAS can operate for many years with no discernable failure (either surcharge or groundwater impacts), while others can fail within weeks of installation, potentially resulting in adverse environmental and public health effects (and economic impacts to the owner). Yet, the evidence to support the argument that SAS cause widespread and serious pollution to surface and more commonly groundwaters, is by no means conclusive.

This paper begins with a review of some key hydrological and biogeochemical mechanisms in SAS including the processes leading to hydraulic failure. Following this, the treatment capabilities of the SAS are discussed drawing on previous investigations. A critical review of the contrasting findings of the contamination potential of septic trench effluent is presented. The paper concludes with a discussion of the key areas of further research in the sustainable management of soil-based wastewater treatment systems.

Hydraulic processes in soil absorption systems

The mechanisms governing purification and hydraulic performance of a SAS are complex and have been shown to be highly influenced by the biological zone (biomat) or ‘clogging layer’ which develops on the soil surface within the trench (Bouma 1975; Siegrist and Boyle 1987). The biomat generally has a low hydraulic conductivity. Bouma (1975) calculated values of approximately 0.6 mm/day for clay soils and 2 mm/day for sandy soils.

The hydraulic conductivity of the biomat reduces over time with a concomitant increase in biomat resistance. With this increase in resistance, flow through the biomat is reduced to an extent that effluent can build up above the biomat while the underlying soil remains unsaturated (Kristiansen 1981a). It is the unsaturated flow characteristics ($K(\Psi)$) of the soil and the resistance properties of the biomat that govern the long-term flow rates through the biomat and sub-biomat zone (Huntzinger Beach and McCray 2003).

A crust-capped soil, as is the case in a mature SAS, has been shown to behave as a “self-adjusting” system, where a steady-state infiltration rate and soil moisture profile develops over

time (Hillel 1980). This steady-state is reached when sub-biomaat soil matric potentials (Ψ) create a gradient across the biomaat, and the unsaturated hydraulic conductivity below the biomaat allows a state of equal flux through both the biomaat and unsaturated zones (Hillel 1980). This condition can be expressed as:

$$Q_b = Q_u = K_b \left(\frac{dH}{dZ} \right)_b = K_u \left(\frac{dH}{dZ} \right)_u \quad (1)$$

where Q_b is the steady-state flux through the biomaat (m/day), Q_u is the steady-state flow through the unsaturated zone below the biomaat (m/d), K_b is the biomaat hydraulic conductivity (m/d), $(dH/dZ)_b$ the biomaat hydraulic gradient, K_u the unsaturated hydraulic conductivity (m/d) and $(dH/dZ)_u$ the hydraulic gradient of the unsaturated sub-biomaat zone.

Low flow rates in absorption systems are not exclusively a result of the interaction between unsaturated soil hydraulic conductivity and biomaat resistance. Dispersion or swelling in sodic soils, resulting from low electrical conductivity and high sodium absorption ratio effluent applications, can substantially decrease soil hydraulic conductivity (Halliwell *et al.* 2001; Patterson 2001). In this case the steady-state flow would be less easily predicted as a factor solely of biomaat zone hydraulic resistance.

The resultant Q in equation 1 is the long-term steady-state flux (m/d) at which, theoretically, a SAS can continue to accept effluent without hydraulic failure occurring. This flux value is also known as the long-term acceptance rate (LTAR), with units of mm/day or L/m²/day. The LTAR is a key parameter used in the Australian and New Zealand Standard AS1547:2000 to

calculate the soil surface area and length of trench required to ensure SAS are not overloaded. The LTAR curve was originally formulated from the work of Brouwer and Bugeja (1983) who carried out a land capability assessment for septic systems in Victoria. The most significant aspect of the report was the development of a curve which plotted the relationship of soil hydraulic conductivity with LTAR of effluent into soil (Brouwer and Bugeja, 1983). This LTAR curve became the basis for sizing recommendations, e.g. trench length/equivalent person, in the Australian Standard publication AS1547:1994 (Standards Australia 1994) and Australian and New Zealand Standard - AS/NZS 1547: 2000 (Standards Australia and Standards New Zealand 2000). Unfortunately, there were a number of limitations with the study, including soil solution sampling difficulties, limited replications, questionable suitability of sites, and unusually dry weather. As a result of these difficulties, only one pair of septic absorption trenches was investigated (Brouwer and Bugeja 1983). The authors acknowledged these issues and emphasised that a more representative dataset would be required to substantiate the conclusions and recommendations made in their report.

Biomat zone genesis and development

Biomat zone genesis and development is a dynamic process which can be influenced by physical, biological and chemical processes. The dominance of any one process can be difficult to isolate as they often occur concurrently (Baveye *et al.* 1998). Biomat genesis is generally characterised by an initial physical clogging of the pores in the infiltrative surface of the native soil (Otis 1984; Siegrist *et al.* 1991). Anaerobic biological activity has commonly been identified as the main subsequent clogging process (Siegrist and Boyle 1987; Tyler and

Converse 1994). Clogging usually occurs within the first few months of full operation of a SAS (Kristiansen 1981a).

The main factors influencing the initial clogging and biomat zone genesis are the wastewater characteristics (suspended solids (SS), biochemical oxygen demand (BOD), and loading rate. Other factors include poor construction practices (smearing of the trench bottom), electrical conductivity, sodium absorption ratio and underlying soil structural and textural properties (Otis 1984). Stimulated by a favourable environment (eg. anaerobic conditions, high humidity and moisture) in the initially clogged soil, biological activity then plays a significant role in long-term growth of the biomat zone (Bouma 1979).

Based on marked reductions in infiltration rate over time, three distinct phases of soil clogging leading to reduction in infiltration rate have commonly been observed (Allison 1947; Jones and Lee 1979; Otis 1984; Siegrist and Boyle 1987). A general pattern of infiltration rate decline adapted from Otis (1984) is presented in Figure 2.

Fig. 2

Phase I of biomat zone development is characterised by a sharp reduction in infiltration rates following effluent application. The initial clogging mechanisms can be attributed to several factors. These include physical straining of organic materials and suspended particulates contained in the wastewater and entrapment of gases (Bouma 1979; Baveye *et al.* 1998; Siegrist *et al.* 2000). These processes act to block soil pores in the infiltrative surface, thus

impeding pore connectivity and flow rate through to the unsaturated zone beneath the absorption system.

Following a sharp reduction in the infiltrative rate during phase I, a more gradual decrease in infiltration rate has been observed (Jones and Lee 1979; Otis 1984; Siegrist and Boyle 1987). Biological activity stimulated by changes to soil conditions created during phase I (eg. low aeration status, high humidity and moisture levels) is believed to be the predominant mechanism of clogging in this second phase (Frankenberger *et al.* 1979; Siegrist and Boyle 1987; Ronner and Wong 1998; van Cuyk *et al.* 2001b).

The third phase of biomat zone development is represented by low infiltration rates where some researchers have observed an equilibrium state (i.e. LTAR) to evolve. During this phase accumulation of clogging materials at the biomat's surface is balanced out by die-off and sloughing of clogging material at the bottom (McGahuey and Winneberger 1964; Bouma *et al.* 1974; Siegrist 1987; Jenssen and Krogstad 1988; Mamedov and Levy 2001). Once established, factors influencing *long-term* growth of the biomat zone include hydraulic ($L/m^2/day$) and organic loading rates (i. e. cumulative BOD and suspended solid), dosing regime (i.e pressure versus gravity) (Rice 1974; Siegrist and Boyle 1987; Stevik *et al.* 1999), aeration status of the infiltrative surface (De Vries 1972; Kristiansen 1981a; Siegrist and Boyle 1987) and the underlying soil biogeochemical properties (Bouma 1975; Kropf *et al.* 1977). Additionally, the temperature of the wastewater being applied to the soil is an influential factor on biomat development (Kristiansen 1981a; Ronner and Wong 1998), with cooler temperatures generally promoting greater biomat development (De Vries 1972; Ronner and Wong 1998).

Seasonal or infrequent use of SAS has also been shown to influence biomat development with only partial growth, or even the absence of a biomat, occurring from infrequent use (Postma *et al.* 1992).

Predicting Long-term Acceptance Rates of SAS

The hydraulic effects of the biomat zone on LTAR (Q) can be predicted if the resistance of the biomat (R_b) and the unsaturated hydraulic conductivity characteristics, $K(\Psi)$ of the underlying soil are known. Bouma (1975) showed that the hydraulic conductivity of the biomat (K_b) is a function of both R_b and the biomat zone thickness (Z_b).

Biomat resistance is the product of the inverse of K_b and the effective thickness of the biomat (Z_b). Taking $K_b(dH/dZ)_b$ from Equation 1 and assuming a steady infiltrating soil profile where the hydraulic gradient approximates unity, we can write:

$$Q_u = K(\psi) = K_b \left(\frac{dH}{dZ} \right)_b$$

Fig. 3.

$$= K_b \left(\frac{H_o + \psi + Z_b}{Z_b} \right)$$

By rearranging this, the hydraulic resistance (R_b) of the biomat can be determined:

$$\frac{K(\psi)}{H_o + \psi + Z_b} = \frac{K_b}{Z_b} \equiv \frac{1}{R_b} \quad (2)$$

where $K(\Psi)$ is the unsaturated hydraulic conductivity of the sub-bioma zone as a function of soil moisture potential, and H_o is the positive hydraulic head on top of the bioma. A definition diagram of Equations 1 and 2 is presented in Figure 3.

Bouma (1975) calculated R_b from measured soil potentials below trenches and reported ranges from 5-7 days for sands, 150 days for silt loams and 45-65 days for clays and silty clays. The variation in values was attributed to differences in porosity, structural instability and biological activity between soils. The wetted perimeter or lower boundary of the saturated bioma is likely to be less abrupt in sandier soils compared with the finer-textured soils. This may have affected the tensiometer readings and hence the calculated R_b values reported in Bouma (1975), particularly if the position of the tensiometers in the soil profile was the same for each soil type.

Beal *et al.* (2004a) used Equation 2 to predict the effect of increasing R_b on flow rates for various Australian soils. Measured moisture retention characteristics ($K-\Psi$) taken from the literature (Forrest *et al.* 1985) were used to predict steady-state fluxes for various bioma resistances and soil textures. The predicted effect of R_b on LTAR is illustrated in Figure 4.

Fig. 4.

The results from Beal *et al.* (2004a) were similar to those of other studies (e.g. Magdoff and Bouma 1974; Huntzinger Beach and McCray 2003) in that a 2 to 3 order of magnitude variation in saturated hydraulic conductivity between soils collapsed to a one order of magnitude variation in LTAR. Sidewall exfiltration of effluent above the ponded bioma was not included in the prediction, thus the LTAR were likely to be conservative.

The area of sidewall that has no impedance from a biomat zone can be referred to as the exfiltration zone and has been shown to be an important pathway for effluent under episodic peak loadings (Beal *et al.* 2004b). There are a limited number of studies modelling unsaturated flow in SAS (e.g Janni *et al.* 1980; Hansen and Mansell 1986; Huntzinger Beach and McCray 2003). Even less widely reported is the specific partitioning of biomat zone and non-bioma zone flow in SAS. A study by Brouwer *et al.* (1979) found flow through the sidewall to be greater than bottom flow in some texture-contrast soils (e.g Kurosols) in Victoria. This conclusion was drawn from field measurement of matric potentials below and adjacent to trenches and the ponded height of effluent in the trenches. The infiltration rate through the sidewalls was calculated at 35mm/day, however it is not clear if sidewall flow was through a biomat zone. Huntzinger Beach and McCray (2003) used HYDRUS-2D to predict unsaturated flow within SAS, and described a strong relationship between the biomat zone hydraulic properties, and the steady-state (long-term) infiltration rates within the unsaturated zone. The model assumed that all flow occurred through either the trench bottom or trench sidewall biomat layer, thus precluding the opportunity to predict flow dynamics for the remainder of the trench sidewall.

Predicting biomat zone development

Although factors influencing biomat development are generally well-known, predicting biomat development itself is difficult. Predicting biomat growth, and thus infiltration rate decline, would allow greater knowledge of the hydraulic capacity and likely treatment efficacy of SAS in various soil types. A clear relationship has been identified between organic loading rate into

the trench (i.e. BOD and SS) and the rate and extent of biomat development (Laak 1986; Siegrist and Boyle 1987). Drawing from this, the concept of pretreating septic tank effluent prior to dispersal into trenches has been investigated, with researchers generally agreeing that this improves the longevity of SAS by inhibiting excessive biomat growth (Laak 1970; Siegrist and Boyle 1987; Converse *et al.* 1998; Harrison *et al.* 2000; Potts *et al.* 2004). Some models have been proposed to quantify biomat development as a function of organic loading rates (Laak 1986; Siegrist 1987). These models have provided a useful basis for predicting biomat development and hence LTAR of SAS. However, the applicability of these models is limited to the specific set of experimental design conditions and wastewater quality associated with the particular study. Consequently, they are unlikely to be reproducible for general estimations of biomat development. (Laak 1986) describes a cube root relationship between infiltration rate, trench (bottom) area and organic loading rate by:

$$A_A = A_s [(BOD_5 + TSS) / 250]^{1/3} \quad (3)$$

where A_A is the adjusted area required (m^2), A_s is the area required for a standard septic system (m^2), BOD_5 is the five day biochemical oxygen demand (mg/L), and TSS the total suspended solids (mg/L). Soil absorption trench design may not be applicable using this relationship as Equation 3 was derived from soil column experiments where highly pre-treated effluent (i.e. low BOD and SS concentrations) was used. Additionally, only permeable soils were used in the soil column experiments.

Siegrist and Boyle (1987), using cumulative organic loading rates, also developed a logistic model formulated from a basic sigmoidal curve function of infiltration rate over time:

$$IR_t = 241 * \frac{\{\exp[2.63 - 5.70(tBOD) + 41.08(TSS) - 0.048(tBOD * TSS)]\}}{\{1 + \exp[2.63 - 5.70(tBOD) + 41.08(TSS) - 0.048(tBOD * TSS)]\}} \quad (4)$$

where IR_t is the infiltration rate at time, t (cm/day), $tBOD$ is the cumulative density loadings (kg/m^2) of total BOD (carbonaceous BOD and nitrogenous BOD), and TSS is total suspended solids (kg/m^2). This model suggests that, ultimately, the infiltration rate would approach zero with continual effluent loading (containing BOD and SS). Although Equation 4 considers cumulative density loadings of organic and inorganic fractions in septic tank effluent, it does not account for the dynamically bioactive nature of the biomat zone.

Weintraub *et al.* (2002) developed a biozone model that considered respiration, mortality and growth of bacteria in the biomat zone as a function of organic matter. The strength of this model is the incorporation of soil physical parameters such as water content and porosity, along with the biological components. However, the link between soil matric potential and unsaturated hydraulic conductivity below the biomat is not evident. Also absent is the key parameter of biomat resistance (thickness / hydraulic conductivity of the biomat). The absence of $K(\Psi)$ as an input parameter weakens the model's predictions of biozone resistance effects.

Overview of treatment performance of SAS

The quality of septic tank effluent is highly variable (Table 1). The least variable of the key effluent pollutants is faecal coliforms which have been consistently reported at concentrations between 10^5 and 10^7 colony forming units (cfu)/mL (Brandes 1978; van Cuyk *et al.* 2001a; USEPA 2002). Virus concentrations in septic tank effluent are less widely reported but could

be expected to be in the range 10^5 to 10^6 counts/100mL F-RNA bacteriophages (viral indicators) (Pang *et al.* 2003).

Table 1. Septic tank effluent quality for key pollutants

Studies suggest that nutrient and pathogen removal mechanisms in the biomat zone, primarily adsorption and filtering, are important processes in the overall purification abilities of a SAS. Table 2 provides a summary of some field and laboratory work on the removal efficiencies by soil with an emphasis on the biomat zone and the first 90 - 200 cm of unsaturated media. This list is by no means exhaustive but highlights some key work that has been done in this area.

The hydraulic and purification processes that occur when effluent passes through the biomat and underlying unsaturated zone are closely linked. Within the unsaturated zone, purification processes include sorption, chemical reactions, biotransformation, pathogen die-off and predation, and plant uptake (van Cuyk *et al.* 2001b). The biomat zone itself is an important component of the purification processes in SAS (Magdoff *et al.* 1974b; Siegrist 1987). The biomat zone can provide optimal conditions for treatment processes described above due to the increased humidity moisture levels and micro-organism populations present (Siegrist *et al.* 1991; Baveye *et al.* 1998).

1 **Table 2**

2

3

4 *Role of unsaturated zone in effluent treatment*

5 Data collated from Table 2 indicates the importance of the unsaturated depth of media in
6 reducing contaminants in effluent, particularly pathogens. High removal rates of effluent
7 pollutants (eg. pathogens, nutrients, organics and SS) in SAS are correlated with the presence
8 of a well developed biomat zone (Magdoff and Bouma 1974; Kristiansen 1981b,c; Van Cuyk
9 *et al.* 2001). Soil chemical characteristics, such as cation exchange capacity and organic matter
10 content, are also important factors influencing the degree of effluent treatment in soil
11 (McCardell and Davison 2003; Al-Shiek Khalil *et al.* 2004; Dawes and Goonetilleke 2004).
12 However, the efficiency of sand media in effluent treatment, particularly the reduction of BOD,
13 SS and pathogens, is also well documented (Crites and Tchobanoglous 1998; van Cuyk *et al.*
14 2001b; Davison *et al.* 2002), despite its high hydraulic conductivity and the relatively low
15 physico-chemical activity of sand.

16

17 The treatment process in a SAS can be likened to the processes which occur in a single-pass
18 sand filter. In a sand filter, effluent is applied intermittently at the top of the sand bed and
19 percolates slowly and evenly throughout the bed. The removal of effluent contaminants occurs
20 mainly in the upper few centimetres of the bed where a biologically active layer is formed
21 (Adin 1998). In a properly functioning SAS, a biomat zone develops at the surface of the soil
22 (bottom of trench) and effluent passes through this biomat and into the unsaturated zone. The
23 presence of a mature biomat will reduce the flow to an extent where unsaturated conditions
24 exist below the biomat, even when there is ponding above the biomat (Fig 5).

25

26

27

Fig. 5.

28 Unsaturated soil conditions create an environment much like a sand filter system, where the
29 unsaturated zone promotes aerobic degradation of pathogens, prolonged retention time of
30 effluent, and maximum contact with the soil media. Despite this analogy, studies suggest
31 treatment efficiencies in SAS are generally inferior to those reported in sand-based treatment
32 systems (Harrison *et al.* 2000; USEPA 2002). Much of the data presented in Table 2 has been
33 generated from experiments or field work on sands or sandy soils. This is a clear limitation in
34 the literature as many of the reported failing and / or poorly operating SAS occur in clay soils,
35 rather than in sandy ones.

36

37 A key difference between an intermittently-dosed sand filter system and a conventional SAS is
38 the inability of a gravity-fed SAS to evenly distribute effluent across the full length of trench
39 bottom. Intermittent pressure dosing of effluent to soil absorption systems has been
40 investigated as a method for improving the aeration status and therefore promoting longevity of
41 a system (McGauhney and Winneberger 1964; Bouma *et al.* 1974; Uebler 1984; Jenssen and
42 Krogstad 1988). Intermittent dosing can avoid saturated conditions where anaerobic bacteria
43 thrive and accumulate at the infiltration surface (Siegrist *et al.* 1983; Bancole *et al.* 2003).
44 Dosing also increases the uniformity of application, thereby reducing the ‘creeping failure’ that
45 is associated with the localised accumulation of solids and organic materials. Oxygen
46 diffusion can also occur more readily, allowing for the aerobic biodegradation of organic
47 materials and improving the air-filled porosity of the infiltration surface (Bancole *et al.* 2003;
48 Potts *et al.* 2004). The mechanisms within the biomat which are responsible for ‘recovery’ are
49 thought to be associated with decomposition of accumulated organic compounds by oxidative
50 respiration, and drying and contraction of microbial by-products (Bouma *et al.* 1974). These

51 processes increase the macropore space within the biomat and allow for greater infiltration.
52 Excessive and localised loading can lead to saturated flow conditions as only a portion of
53 surface area available for effluent dispersal is utilised. In the United States, technologies such
54 as pressure distribution systems are quite commonly incorporated into conventional SAS to
55 improve the distribution of effluent into the trenches / beds (Siegrist *et al.* 2000). However, in
56 Australia this method for improving system performance has not been so readily adopted -
57 although pressure dosing trenches / beds is referred in the Australian and New Zealand
58 Standard as a method to ensure uniform application (Standards Australia and Standards New
59 Zealand 2000).

60

61 Gas composition in the vadose zone of a SAS is important in the treatment capacity of the
62 system and in its long-term hydraulic functioning (Kristiansen 1981a; Wilhelm *et al.* 1994a;
63 Potts *et al.* 2004). There are several investigations (Magdoff *et al.* 1974a; Magdoff *et al.*
64 1974b; Gerritse *et al.* 1995a; Cromer 2001) that demonstrate that aerobic and oxic conditions
65 prevail under trench systems, despite the often saturated nature of the system and the anaerobic
66 character of septic tank effluent. The presence of oxygen, carbon (C) and form of nitrogen (N)
67 determines the composition of the microbial population (aerobic and anaerobic) responsible for
68 effluent treatment. For example, nitrification of ammonium-N to nitrate will only occur in the
69 presence of oxygen and aerobic bacteria. High rates of complete or near complete nitrification
70 in the unsaturated sub-biomat zone in trenches or soil column experiments have often been
71 reported (Walker *et al.* 1973a; Pell and Nyberg 1989b; van Cuyk *et al.* 2001b).

72

73 In soil column experiments, Magdoff *et al* (1974a, 1974b) demonstrated that columns with a
74 developed biomat and perforated sides to allow air exchange, had similar N, C, and phosphorus
75 (P) transformations as columns that had no perforations but had no biomat development.
76 Conversely, columns that had biomat development but no perforations to allow air exchange
77 had lower levels of N, P and C transformation, particularly N where almost 100% of the
78 leachate was in the ammonium form (Magdoff *et al.* 1974b).

79

80 *Organic matter and suspended solids*

81 In addition to promoting an aerobic soil environment through the establishment of unsaturated
82 conditions, the biomat acts as a filter in straining and trapping biodegradable organics,
83 measured as BOD and SS. The biomat itself is composed partly of organics and SS originating
84 from septic tank effluent (Bouma 1979; Laak 1986; van Cuyk *et al.* 2001b). High removal
85 rates of BOD and SS, ranging from 70% to 95%, have been consistently reported in the
86 literature (Daniel and Bouma 1974; Pell and Nyberg 1989a; van Cuyk *et al.* 2001b).

87

88 *Pathogens*

89 The fate of pathogens (eg. bacteria and viruses) from domestic wastewater has been widely
90 investigated in both field and laboratory environments. The pathways for pathogen export from
91 SAS are surface water run-off from surcharging (hydraulically failing) trenches or groundwater
92 intrusion via saturated flow beneath a trench. Risk of human contact with pathogens from on-
93 site systems generally increases with decreasing temperature, saturated and anaerobic soil
94 conditions (Reneau *et al.* 1975; Yates and Yates 1988; Beavers and Gardner 1993; Powelson
95 and Mills 2001). Pathogen populations are reduced dramatically by passage through 60 cm –

96 90 cm of unsaturated soil under the biomat zone (Kristiansen 1981c; Powelson *et al.* 1990;
97 Stevik *et al.* 1999; Siegrist and Van Cuyk 2001; Pang *et al.* 2003; van Cuyk *et al.* 2004).
98 Substantial reductions (\leq log 3-5 decreases) in bacteria concentrations within 90 cm depth of
99 unsaturated media have been reported (Rahe *et al.* 1978; Anderson *et al.* 1994; Weiskel *et al.*
100 1996; van Cuyk *et al.* 2001b; Pang *et al.* 2003). Population reductions of >99% for viruses
101 have been reported in 60 cm of unsaturated sand (Higgins *et al.* 1999; Oakley *et al.* 1999;
102 Siegrist and Van Cuyk 2001). Weiskel *et al.* (1996) found that although faecal coliforms from
103 SAS contributed the greatest potential load in the Buttermilk Bay catchment, significant
104 subsurface attenuation (4-5 log removal) within the vadose zone 1 – 2 m down gradient of the
105 SAS, resulted in an estimated 0.01% load into the Bay. Many of these studies were done in
106 sandy soils where an unsaturated zone is more likely to occur under a trench due to a greater
107 fraction of air-filled void space due to draining of large pores. However, good pathogen
108 removal rates have been reported in finer-textured soils, for example Oakley *et al.* (1999)
109 reported 100% removal of MS2-coliphage in 60 cm of clay loam.

110

111 The biomat zone itself plays a greater role in the removal of pathogens from the wastewater
112 stream than it does in the removal of nutrients (van Cuyk and Siegrist 2001). While the
113 anaerobic conditions in the biomat zone are not favourable for inactivation, pathogen removal
114 is facilitated in the biomat zone by straining and adsorption processes. Whelan and Parker
115 (1981) reported a marked reduction of faecal coliforms within approximately 30cm below the
116 biomat zone of a SAS located in a in a sandy soil.

117

118 Alhajjar *et al.* (1988) reported that filtering in the biomat zone effectively removed bacteria,
 119 but not the much smaller poliovirus; although the biomat zone appeared to at least retard the
 120 passage of poliovirus into the ground water. Both Bouma *et al.* (1972) and Van Cuyk *et al.*
 121 (2001) observed high densities of coliform bacteria in the biomat zone (approximately 15-20
 122 mm thick). Lysimeter experiments have demonstrated an association between the stage of
 123 biomat development and pathogen removal percentage, where a proportional increase in
 124 removal rates occurred as the biomat matures (van Cuyk *et al.* 2001b). However, it is unclear
 125 whether this relationship was tested for statistical significance. In van Cuyk *et al.*'s study, viral
 126 die-off through the unsaturated zone was calculated by a one-dimensional model where
 127 microbial die-off is described as:

128

$$129 \quad C_t = C_o \exp(-kt) \quad (5)$$

130 where C_t is the concentration of viruses at time, t (days), C_o is the initial concentration of
 131 viruses (pfu/mL) and k is the first-order rate co-efficient for net die-off rate of viruses.

132

133 The retention time in the vadose zone was described as:

134

$$135 \quad t = \frac{\text{SoilDepth} \times \text{EffectivePorosity} \times \text{EIS}}{\text{EffluentApplicationRate}} \quad (6)$$

136

137 where EIS is the effective infiltration surface which is 1 for a mature trench and 0 for a new
 138 trench (van Cuyk *et al.* 2001b). Van Cuyk *et al.* (2001) used Equations 5 and 6 to investigate
 139 whether the type of infiltrative surface (e.g. gravel versus gravel-free sand lysimeters) was
 140 important in the treatment efficiency. The authors found comparable treatment efficiencies

141 between the two surfaces, and suggested that hydraulic retention time and proportion of surface
142 utilised was more important than the type of surface. This paper drew a credible link between
143 hydraulic processes and treatment efficiency, and illustrated the importance of the first few
144 centimetres, including the biomat zone, in SAS performance.

145

146 Pathogen removal in SAS is well-studied and generally understood in terms of the need for an
147 unsaturated zone for effective treatment of effluent. Without this vadose zone, the chances of
148 pathogens contaminating groundwaters are much higher. Pathogen pollution into surface
149 waters (via run-off) in non-sewered areas has also been explored (Geary 1992; Heisig 2000;
150 Graves *et al.* 2002; Ahmed *et al.* 2005). It can be difficult to unambiguously determine the
151 contribution from on-site systems to pathogen pollution due to difficulties in identifying other
152 sources of faecal pollution (e.g. birds and animals). However, there is an increasing number of
153 water quality studies using methods to differentiate between human and non-human sources of
154 faecal pollution, as discussed in more detail later.

155

156 *Nitrogen*

157 Several factors influence how effectively N is assimilated in the soil. The redox status, soil
158 microbial composition and labile C source are the key factors which determine the degree of
159 total N removal in a SAS (Wilhelm *et al.* 1994a; EPRI 2000). The main form of N in septic
160 tank effluent is ammonium (Whelan and Titamnis 1982) and this commonly undergoes rapid
161 nitrification once the effluent leaches into the unsaturated, aerobic zone underlying the biomat
162 zone (Aravena *et al.* 1993; Wilhelm *et al.* 1994b; Aravena and Robertson 1998). Removal of
163 nitrate, the product of nitrification, is not efficient in the aerobic, low C soil conditions of the

164 unsaturated zone as these conditions inhibit denitrification and subsequent gaseous loss of N.
165 Whelan and Barrow (1984a) found that nitrification was inhibited by the anaerobic state of the
166 biomat layer, but once the effluent passed through the biomat, nitrification was almost
167 complete within half a metre. Other researchers have described similar results with virtually
168 complete nitrification occurring within a few centimetres of the bottom of the biomat zone
169 (Walker *et al.* 1973b; Kristiansen 1981b; Cogger *et al.* 1988; Pell and Nyberg 1989b; Gerritse
170 *et al.* 1995b). Nitrogen can also be physically removed from the effluent via filtration through
171 the biomat as observed by Magdoff and Bouma (1974). They found high concentrations of
172 organic N at, and just below, the infiltrative surface layer of clogged soil columns where a
173 biomat was present compared with columns where there was no biomat present (Magdoff and
174 Bouma 1974). Under anaerobic conditions (i. e. no opportunity for conversion to nitrate),
175 ammonium adsorption can occur (Harrison *et al.* 2000) particularly for soils with a high cation
176 exchange capacity e.g. montmorillonitic soils (McCardell and Davison 2003).

177

178 Although removal of total N in SAS is generally not efficient, due to the absence of a
179 significant denitrification phase, there is some evidence to suggest N removal by SAS can
180 occur. Dawes and Goonetilleke (2003) reported that the greatest improvement in water quality
181 occurred within 1m of absorption trenches (sample size 16 SAS) with negligible further
182 removal between 1-3m from trench. Data was not given on the removal rates between the
183 trench and the piezometers located 1m from the trench, though this data would have been
184 useful. Cromer (2001) reported markedly reduced nitrate concentrations within 10 m to 20 m
185 from the trench located in a sandy soil in Hobart, Tasmania. Unfortunately only one SAS was
186 investigated in this study, thus limiting the comparison of these results with similar coastal

187 environments. Gerritse *et al.* (1995b) using a mass balance of inorganic N and bromide,
188 reported $\approx 80\%$ of N was lost within 10 m of travel in sandy soil in Peth, Western Australia.
189 They concluded that N additions to catchment waterways were originating to a much greater
190 extent from agricultural areas compared to non-sewered areas (Gerritse *et al.*, 1995b).

191

192 In general though, loss of N from SAS is usually poor and elevated nitrate concentrations in
193 groundwater associated with SAS have been well-documented (EPRI 2000). Tracer
194 experiments have revealed that nitrate can travel in aquifers underlying SAS in relatively well-
195 defined, narrow plumes which have been recorded to be up to 130 m in length (Robertson *et al.*
196 1991) but may extend up to 200 m (Valiela *et al.* 1997).

197

198 *Denitrification*

199 In the absence of oxygen, nitrate can be lost from the system by denitrification, providing a
200 supply of labile C is available. Optimal conditions for denitrification are generally limited to
201 small anaerobic pockets in the vadose zone or the biomat itself, therefore N removal is
202 generally low in SAS (Reneau *et al.* 1975; Wilhelm *et al.* 1994a). However, with their source
203 of labile C and often anaerobic soil conditions, riparian zones, can help to reduce nitrate
204 concentrations in (shallow $\leq 2\text{m}$) groundwater that intercepts this zone (Robertson *et al.* 1991;
205 Hill 1996; Anderson 1999; Gold *et al.* 1999).

206

207 Denitrification in riparian zones has been reported to be both spatially and temporally variable
208 (Gold *et al.* 1999). Robertson *et al.* (1997) studied plumes from SAS in sandy soils and found
209 that over time, SAS-derived nitrate concentrations in receiving waters were much lower than

210 expected, and concluded that denitrification in the riparian zone was a key removal mechanism
211 for nitrate. Geary (2004) demonstrated the importance of downstream riparian zones in his
212 reporting of substantial nitrate losses between an absorption trench and an adjacent surface
213 water body. Groundwater nitrate concentrations decreased from a mean of 75 mg/L to a mean
214 of 2.8 mg/L over a distance of approximately 3 m (Geary 2004). A riparian strip was situated
215 between the two monitoring points, and Geary (2004) suggested that nitrate loss was from
216 plant uptake, denitrification and possibly dilution from converging groundwater flows.
217 Chemical denitrification can also occur in certain soils, for example the oxidation of pyrite,
218 using nitrate as an electron acceptor, will produce nitrogen gas (Postma *et al.* 1991).

219

220 *Phosphorus*

221 The main form of P in septic tank effluent is orthophosphate. The geochemical mechanisms
222 influencing the availability of P in and below SAS are adsorption/desorption,
223 precipitation/dissolution and biological immobilisation (EPRI 2000). Most studies indicate
224 that P removal in SAS is generally effective (Brouwer and Bugeja 1983; Gerritse 1993;
225 Wilhelm *et al.* 1996; Robertson and Harman 1999). In general, soils (including many sandy
226 soils) have the capacity to retain P (Jones and Lee 1979; Weiskel and Howes 1992).

227

228 While the role of the biomat on P removal is poorly understood, clearly some retention of P
229 would occur during the development phase of the biomat zone. Phosphate removal is certainly
230 indirectly influenced by the biomat, if not directly. Sub-biomat soil conditions such as redox
231 and pH, which are important in P retention processes, are influenced substantially by the extent
232 of biomat development. Magdoff *et al.* (1974b) found greater P removal in soil columns with

233 well developed biomats compared to columns with poorly developed or absent biomats.
234 Changes to pH conditions in and just below the biomat were suggested as one factor
235 contributing to this difference.

236

237 Phosphate is more strongly retained by the soil matrix under conditions of high pH and
238 oxidation status (Ponnamperuma 1972), conditions which are more likely to prevail in an
239 aerobic, unsaturated environment that is promoted by the presence of an overlying biomat
240 zone. Localised P enrichment can lead to slow release of P into groundwaters over the long-
241 term, though has only been reported for sandy soils (Whelan and Barrow 1984b; Gerritse *et al.*
242 1995a). Calcareous sands however, have been reported to have a good ability to retain P via
243 rapid sorption then slow precipitation of phosphate with calcium to form amorphous crystalline
244 minerals (Wilhelm *et al.* 1994a). Soils containing high sesquioxide (iron and aluminium
245 hydrous oxides) fractions can strongly adsorb P (Menzies *et al.* 1999; Redding *et al.* 2002).
246 Precipitation of calcium and iron phosphates have also been observed below SAS (Whelan and
247 Barrow 1984b). Saturation of soils, or soils exposed to alternate wetting and drying cycles, of
248 which both scenarios may occur in SAS, will also influence P retention. Ptacek (1998) and
249 Zanini *et al.* (1998) describe the influence of suboxic and oxic regions on P within the subsoil
250 and aquifer zones below SAS. For example, Ptacek (1998) describes the elevated presence of
251 vivianite, an amorphous ferric phosphate, which has been formed following dissolution and
252 subsequent precipitation in the more reduced lower zones of the aquifer.

253

254 The influence of micro-scale characteristics in the biomat, vadose and aquifer zone on nutrient
255 assimilation is really only superficially understood in terms of the long term treatment capacity

256 of SAS. Gold and Sims (2000) describe several areas of nutrient dynamics in SAS which
257 require further research, particularly in the context of developing a risk-based model for SAS
258 design and siting.

259

260 **Environmental and human health impacts associated with on-site systems**

261 Both hydraulic and treatment failures can occur from a poorly operating SAS. *Hydraulic*
262 failure (surcharging) occurs when the infiltration rates through the biomat are exceeded by the
263 loading rate of effluent into the trench, resulting in effluent discharge onto the soil surface.
264 Field studies have identified this as a relatively common occurrence for older and / or poorly
265 designed SAS (Brouwer *et al.* 1979; Geary 1994; Dawes and Goonetilleke 2001). *Treatment*
266 failure is less obvious and is linked closely with the soil biogeochemical processes governing
267 the hydraulic behaviour in the soil system (Siegrist and Van Cuyk 2001). A shallow water table
268 and / or saturated subsoil can result in inadequately treated effluent entering the groundwater.
269 The shortened hydraulic retention time and reduced aerobic conditions that occur in these
270 circumstances preclude adequate treatment of effluent prior to contact with groundwater. Both
271 forms of failure may ultimately result in effluent pollutants (nutrients and pathogens) being
272 exported from the application area and entering surface and / or groundwaters (see selected
273 studies in Table 3).

274

275 **Table 3**

276 *Environmental impacts*

277 The pollutants of key environmental concern are N and P. Nutrient enrichment of a freshwater
278 body can lead to accelerated eutrophication. Land use practices such as agriculture and
279 horticulture, are well studied sources of contaminant loads into catchments (Kookana *et al.*
280 1998). However, non-sewered areas have also been shown to contribute to catchment nutrient
281 loads (Valiela and Costa 1988; Weiskel *et al.* 1996).

282

283 Clear hydraulic links have been made between on-site wastewater dispersal practices and
284 nutrient contamination of ground and surface waters (Table 3) with the use of tracers such as
285 bromide (eg. Robertson *et al.* 1991), chloride (e.g. Stewart and Reneau 1988), ¹⁵N stable
286 isotopes (eg. Chen and Harkin 1998), sterol biomarkers (eg. Leeming *et al.* 1996), and viral
287 tracers (eg. Paul *et al.* 1995). All of these studies have found some causal link between
288 elevated effluent-derived pollutant in groundwaters and OWTS, specifically septic systems. It
289 is the *degree* and *impact* of contribution to ground and surface water contamination that
290 remains ambiguous in these studies. The extent of contamination is extremely variable and can
291 be a function of soil type and unsaturated soil depth, existing quality of water body, OWTS
292 density and distance to receptor, groundwater flow velocity, climate and seasonal factors, and
293 age and design of system.

294

295 *Human health impacts*

296 Concern over microbiological contamination from SAS, particularly in groundwater, has been
297 rising over the years, but as Van Cuyk and Siegrist (2001) suggest, this appears to be based on
298 the widespread distribution of on-site wastewater systems, rather than documented evidence.

299 Where there have been reports of SAS-related waterborne disease outbreaks, these have
300 usually been localised and associated with a single poorly performing system (Yates and Yates
301 1988; Cliver 2000; Bopp *et al.* 2003) (Table 3). Cumulative impacts and catchment-wide
302 pathogen loads in non-sewered areas have not been adequately investigated and / or reported.
303 Obviously, there are economic and logistical difficulties in quantifying the origins of a specific
304 diffuse-source pollutant, although catchment water quality models have proved a useful tool in
305 this regard (Yates and Yates 1988; Tong and Chen 2002; Weintraub *et al.* 2002; Whitehead *et*
306 *al.* 2003).

307

308 Several studies have considered cesspools, leaching pools and injection wells as sources of
309 pollution (Table 3) as well as the conventional SAS (Vaughn *et al.* 1983; Chen 1988; Dillon *et*
310 *al.* 2000). Unlike SAS, cesspools and injection wells are not specifically designed to interact
311 with the soil as part of the key treatment process and they are therefore more likely to provide a
312 substandard level of treatment (USEPA 2002). Despite this, they are commonly grouped in
313 with SAS statistics on failure or poor performance of ‘septic systems’ (Craun 1985; Dillon *et*
314 *al.* 1999; USEPA 2002).

315 The number of drinking water-associated disease outbreaks in the United States decreased from
316 39 during 1999-2000 to 31 during 2001—2002 (Blackburn *et al.* 2004). These 31 outbreaks
317 caused illness among an estimated 1,020 persons, with 52 people (5.5%) becoming ill from
318 drinking groundwater in ‘individual’ homes which were presumably non-sewered (Blackburn
319 *et al.* 2004). Assuming these 52 cases were in non-sewered areas, this represents about 7×10^{-5}
320 % of the non-sewered population in the United States (on the basis that 23% of the population
321 lives in non-sewered areas (USEPA 2002)). Outbreaks associated with private wells remained

322 relatively stable, although there was an increase in reporting of outbreaks involving private,
323 treated wells during 2001—2002 (Blackburn *et al.* 2004).

324 The contaminant that is repeatedly found in elevated concentrations in groundwaters down
325 gradient from SAS is nitrate (Robertson *et al.* 1991; Harman *et al.* 1996; Robertson *et al.* 2000;
326 Steffy and Kilham 2004). Despite this, it is interesting to note that very few reports of nitrate
327 toxicity associated with SAS are present in the literature. L'hirondel and L'hirondel (2002)
328 critically examined the evidence for well-water induced methaemoglobinaemia. They
329 concluded that there was a poor correlation between high concentrations of nitrates in well-
330 water and infant methaemoglobinaemia (blue-baby syndrome), with the cases of infant
331 methaemoglobinaemia almost completely absent in the US since 1960 (L'hirondel and
332 L'hirondel 2002). Elevated nitrates in well-water have been linked to privies and cesspools but
333 there is scant mention of the conventional SAS being linked to well-water
334 methaemoglobinaemia. Obviously there is much evidence reporting elevated groundwater
335 nitrate concentrations from SAS, however the assumption that these elevated nitrate levels
336 from SAS are a human health problem should not be automatic and there appears to be little
337 recent scientific evidence to support this assumption.

338

339 **Australian studies**

340 In 1997 over 400 people contracted *Hepatitis A* from eating suspected sewage-contaminated
341 oysters from Wallis Lake (Ryan v Great Lakes Council 1999), triggering the formation of the
342 SepticSafe programme by NSW Department of Local Government. There have been several
343 studies in Australia investigating the contamination of surface and groundwaters from septic
344 systems before and after the Wallis Lake incident (Geary 1994; Hoxley and Dudding 1994;

345 Jelliffe 1998; Whitehead and Geary 2000). A common problem with many investigations into
346 SAS impacts in Australia are the poor datasets and / or evidence of clear links to SAS as the
347 source of contamination.

348

349 A study of two rural towns in Victoria reported variable concentrations of nitrate and faecal
350 coliforms in shallow groundwater below areas of high SAS densities (Hoxley and Dudding
351 1994). However, most of the data which was discussed was not presented in the paper. The
352 authors concluded that “other towns or cities that have septic tanks in densities similar.. are
353 most likely causing nitrate and bacteriological contamination of the local groundwater...”
354 (Hoxley and Dudding, 1994). This conclusion is highly generalised and very likely to be
355 inaccurate given the wealth of literature that demonstrates treatment in SAS is determined by a
356 number of factors including site and soil conditions, system type, loading rates and depth to
357 groundwater (length of vadose zone).

358

359 Sampling and monitoring of surface water, downstream of non-sewered communities on
360 Scotland Island, NSW, showed high concentrations of faecal coliform and enterococci
361 (Martens and Geary 1999). These results, together with sampling and testing of effluent in
362 absorption trenches, led the authors to conclude that the transportation of poorly treated septic
363 tank effluent into surface waters resulted in excessively high bacterial concentrations (Martens
364 and Geary 1999). However, the report did not clearly state the number of water quality
365 samples taken, or if other land use practices and sources of bacterial pollution were considered.
366 Additionally, sampling methods for the drainfield water quality samples were unclear. The
367 results provided appear to indicate that the effluent is of primary treated quality, which

368 suggests that the samples were taken (prematurely) in the saturated zone within the trench
369 itself, rather than the underlying vadose zone where treatment predominantly occurs.

370

371 In southeast Queensland the majority of septic systems use separate greywater and blackwater
372 treatment and dispersal (Beal *et al.* 2005). Beal *et al.* (2005) identified the key management
373 issues in the region as the frequency of greywater failure and inappropriate greywater
374 discharge, and suggested that the common practice of discharging effluent into streams, gutters
375 and drains (Jelliffe *et al.* 1995; Beal *et al.* 2005) may be making the greatest contribution to
376 OWTS-related water quality impacts.

377

378 To date, only a few Australian investigations have been able to demonstrate conclusive
379 evidence of pollution of groundwater by on-site systems. The contribution of on-site systems
380 to poor surface water quality is even more ambiguous. This can, in part, be attributed to the
381 difficulties associated with quantifying diffuse pollution sources. It can also be difficult to
382 clearly determine the contribution from on-site systems to pathogen pollution due to
383 difficulties in separating human-sources from other sources of faecal pollution (e.g. birds and
384 animals). However, there is an increasing number of studies using methods to differentiate
385 between human and non-human sources of faecal pollution. Recent work using 'biomarkers' as
386 a method of distinguishing human faecal contamination from that of other animals is gaining
387 impetus as a useful tool for assessing water quality impacts to catchment water quality,
388 particularly from diffuse sources such as on-site wastewater systems and agricultural land use
389 (Apte and Bately 1992; Leeming 1998; Geary and Davies 2004). Data obtained from such

390 studies will provide more certainty of the role on-site systems play in catchment water quality
391 degradation.

392

393 In areas where shellfish such as oysters are farmed for human consumption, the risks of human
394 health impacts from faecal contamination are increased. Oysters, being filter feeders, are
395 particularly vulnerable to bioaccumulation of contaminants due to their highly efficient
396 filtering capacity compared with humans, for example Pacific oysters can filter up to 50L of
397 water per day (Bayne *et al.* 1999). Geary and Davies (2004) used bacterial source tracking in
398 the shellfish farming region of Port Stephens, NSW, to determine the source of faecal
399 streptococci isolates. They reported that although there was no one source that was statistically
400 significant, SAS were considered one human source of faecal streptococci.

401

402 Ahmed *et al.* (2005) used biochemical fingerprinting to identify unique *E. coli* and enterococci
403 phenotypes in a south-east Queensland waterway. A total of 151 unique biochemical
404 phenotypes, that were identified from 48 septic tanks, were found in Eudlo Creek downstream
405 of a non-sewered area. Of these septic tanks, 23 had absorption trenches that were classified as
406 'soggy' (surface surcharging) and 32 required desludging during the study (Ahmed *et al.*
407 2005). Unfortunately, the testing is not quantitative so it is impossible to ascertain whether
408 these phenotypes were substantial contributors to the total faecal contamination load in the
409 creek.

410

411 The actual *impacts* (e.g. disease, eutrophication, nitrate toxicity) from on-site effluent-polluted
412 waterways are poorly documented. For example, there are few reported cases of outbreaks of

413 endemic illness (Table 3) in areas of high system density and permeable soils; though this
414 would be expected if serious groundwater contamination was present; as was purported to be
415 the case by Hoxley and Dudding (1994). It is acknowledged however, that reporting depends
416 on whether the illness is notifiable or reportable. Absence of evidence is obviously not
417 evidence of absence, and the need for well-considered, long-term water quality monitoring in
418 non-sewered areas is essential to build up an accurate picture of the location, number, and
419 degree of failing on-site systems. This is becoming particularly pressing in areas of high
420 density non-sewered development located near sensitive water receptors and / or on shallow
421 aquifers. Water quality monitoring programmes which generate useful data are difficult to
422 undertake. Event-based monitoring, in addition to baseflow monitoring, is essential as
423 significant surface export of effluent contaminants is only likely to occur during storm events.
424 As discussed, human-sourced faecal pollutants need to be separated from other animals, and
425 SAS-derived nitrate also needs to be discriminated from that arising from other land uses. In
426 this respect, using δN^{15} may be applicable (Steffy and Kilham 2004).

427

428 **Density of on-site systems**

429 A key factor in sustainable OWTS management is providing sufficient lot area for pollution
430 reduction. As the density of on-site systems increases, there is greater potential for adverse
431 impacts such as cumulative water quality contamination (nitrates) and groundwater mounding
432 (Siegrist *et al.* 2000). Allotment density is determined largely by the horizontal (and vertical)
433 setback distances required in each lot in order for sufficient assimilation of effluent pollutants
434 to occur. Research generally suggests that as OWTS density increases, pollutant loads (e.g
435 nitrates and pathogens) in ground waters have also increased (Perkins 1984; Yates 1985;

436 Tuthill *et al.* 1998; Lipp *et al.* 2001). Hence, on-site system density is becoming a critical issue
437 in rapidly developing non-sewered areas, and there is a need to determine sustainable lot
438 densities, although this is an inherently difficult task to undertake. A major problem in
439 determining minimum setback distances from on-site systems is estimating the proportion of
440 off-site export of contaminants due to pollutant concentration reduction and reinfiltration,
441 which will vary from site to site.

442

443 Despite the difficulties there have been some attempts to quantify minimum lot densities
444 (Perkins 1984; Yates 1985; Geary and Gardner 1998; Jelliffe 1999). A density of greater than
445 15 systems /km² is quoted as being unsustainable, although as Whitehead *et al.* (Whitehead *et*
446 *al.* 2001) point out, this is based on very limited data. Jelliffe (1998) suggested that setback
447 distances to contain surface exports should vary with soil type and the target receiving water
448 quality objectives, and proposed a relatively simple biophysical model to calculate sufficient
449 nutrient assimilation area. A summary of some minimum lot sizes and densities recommended
450 in the literature is provided in Table 4.

451

452

Table 4

453

454 There is considerable variation between what is considered a sustainable lot size (Table 4).
455 This is partly due to the variety of factors determining the assimilative capability of a site,
456 partly due to the environmental sensitivity of the area, and partly a result of inadequate
457 knowledge of treatment processes / removal efficiencies of on-site systems.

458

459 **Areas of further research**

460 The 'National Research Needs' Conference held in the United States in 2000 aimed to identify
461 and discuss essential research areas for on-site wastewater management (EPRI 2000). Many of
462 the identified research needs also apply in Australia, including the development of sound risk-
463 based decision making tools, greater understanding of the interactions between hydraulic and
464 treatment mechanisms in SAS, pathogen pathways and removal processes, and the
465 minimisation of nitrate export to groundwater. Some key research areas which can be
466 identified from this literature review are summarised in Table 5.

467

468

Table 5.

469

470 Many of the studies presented in Tables 2 and 3 were undertaken in sandy media, with medium
471 to low clay content. Obviously soils are highly variable and more research across a range of
472 soils types would benefit our understanding of hydrology and treatment processes occurring,
473 not only in SAS, but also on soils being irrigated with secondary effluent from alternative on-
474 site systems.

475

476 Greater knowledge of the biomat zone development, and its interaction with oxygen
477 availability and subsequent N and pathogen transformations, would be a useful advance in
478 predicting the long-term performance of SAS. Research into improvements in nitrate reduction
479 in the sub-bioma zone, is essential for the sustainable future of SAS.

480

481 Identifying and evaluating the potential risks to receiving water bodies from on-site systems is
482 becoming an increasingly popular management approach (Jones *et al.* 2000; Whitehead *et al.*

483 2003; Day 2004). Risk assessment concepts have been implicitly included in regulatory
484 guidelines for many years; for example, the imposition of setback distance criteria of an OWTS
485 to a boundary or sensitive receptor. However, setback distances are site-specific and a risk-
486 based management approach could help to determine suitable setback distances and sustainable
487 OWTS densities at a site and catchment scale. A good risk assessment would also consider
488 cumulative impacts from on-site systems; something which has received little attention in the
489 literature, or from regulators. Research into risk assessment models is being undertaken to
490 investigate their viability and applicability as a tool in onsite system risk assessment. These
491 include the On-site Sewage Assessment Risk Assessment System (OSRAS) (Whitehead *et al.*
492 2003), the Development Assessment Module (DAM) (McGuinness and Martens 2003) and a
493 Quantitative Microbial Risk Assessment (Charles and Ashbolt 2004).

494

495 **Summary**

496 The mechanisms governing purification and hydraulic performance of a SAS are complex and
497 have been shown to be highly influenced by the biomat zone which develops on the soil
498 infiltrative surface within a SAS. The physical, chemical and biological processes that occur in
499 the biomat zone and underlying unsaturated zone are complex and dynamically interactive.
500 Hydraulic and purification processes do not occur separately from each other but interact in a
501 complex, yet potentially predictable way. Equations defining the theoretical movement of
502 effluent through barriers and unsaturated soil zones have been described (eg. Bouma 1975),
503 and more recently, attempts have been made to predict soil clogging development (Siegrist and
504 Boyle 1987; Weintraub *et al.* 2002) and to model the clogging zone impact to flow (Huntzinger
505 Beach and McCray 2003; Beal *et al.* 2004b).

506

507 Laboratory studies involving soil columns and lysimeters, designed with an increasing degree
508 of complexity, have yielded many valuable insights and illuminated our understanding of soil-
509 effluent relationships in various media. Field investigations have, in many cases, validated the
510 results and theories from laboratory studies. Field surveys have identified commonalities in
511 hydraulic failure (poor design, low permeable soil, severe clogging) and purification failure
512 (shallow water table, highly permeable soil, shallow depth of unsaturated zone) between SAS.
513 Although there has been considerable research in the area of on-site wastewater management
514 and soil-based treatment systems, some key processes remain unclear.

515

516 Key treatment processes, occurring in the unsaturated zone beneath a SAS are oxidation,
517 adsorption, pathogen die-off, and ion exchange. Studies of effluent plumes under SAS, and
518 water quality monitoring in non-sewered areas, suggest that on-site systems are contributing to
519 poor water quality. Nitrate and faecal pollution are the two major effluent contaminants.
520 Groundwater nitrate concentrations have been widely reported in non-sewered areas,
521 particularly in high allotment densities on permeable soils and / or shallow water tables. The
522 contribution of on-site systems to catchment pollutant loads and cumulative water quality
523 effects is less clear. In this respect, targeted water quality monitoring, identified from a risk
524 assessment process, is recommended to improve our knowledge of pollution potential of on-
525 site systems.

526

527 In terms of future research, a greater understanding the interactions between hydraulic and
528 treatment mechanisms, and the biomat and sub-bioma zone gas composition including its role

529 in effluent treatment is needed. Improved N removal in SAS remains a priority. Further work
530 on the role of the riparian zone in the reduction of nitrates and the design of systems that
531 incorporate C enriched layers (e.g. Bedessem *et al.* 2005) is necessary. The critical lot density
532 in non-sewered areas is not well understood and consequently setback distances are often
533 unjustified and conservative. Improving our knowledge of micro-scale and site scale processes
534 will lead to a greater understanding of catchment scale impacts from on-site systems.

535

536

537

538

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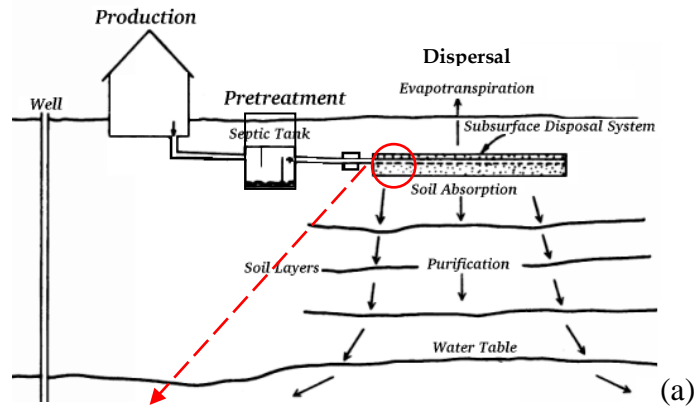
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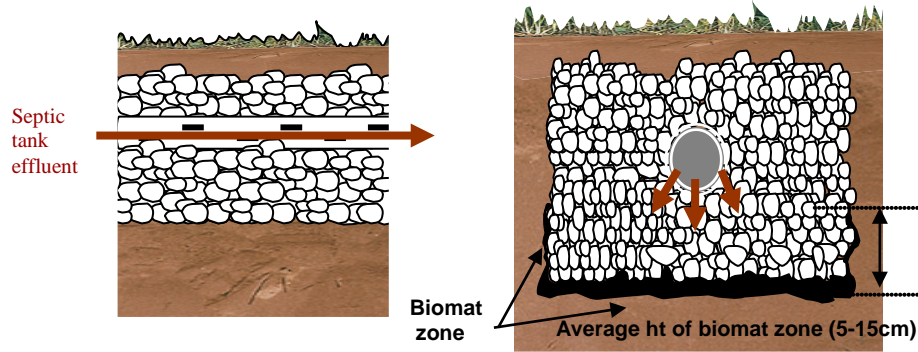
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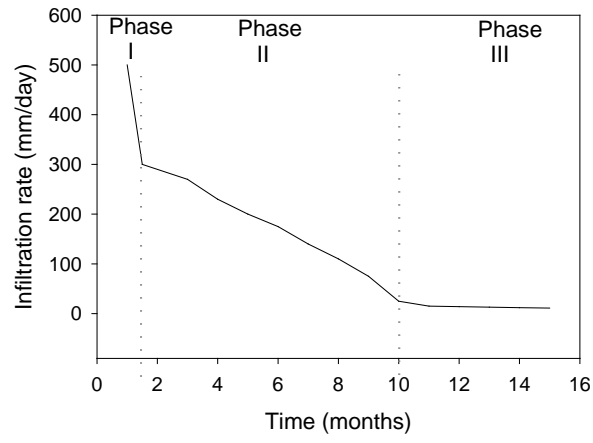


(b) Plan view of distribution pipe in gravel trench

(c) Cross section of distribution pipe in gravel trench

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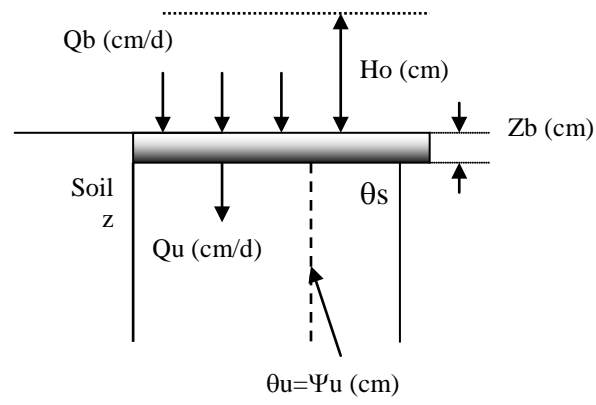
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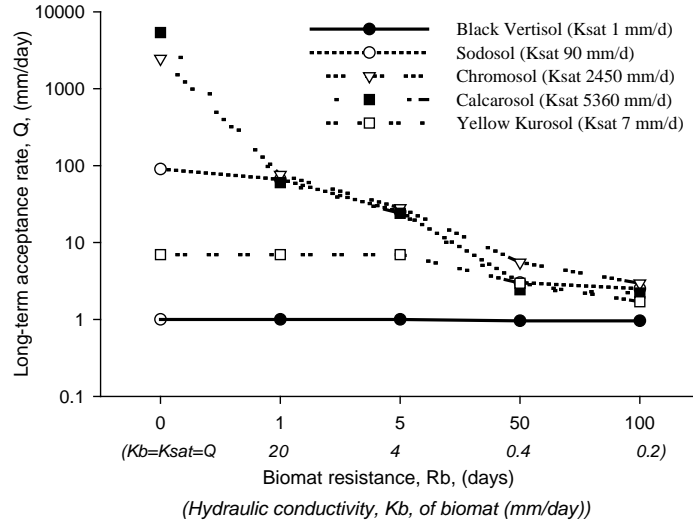
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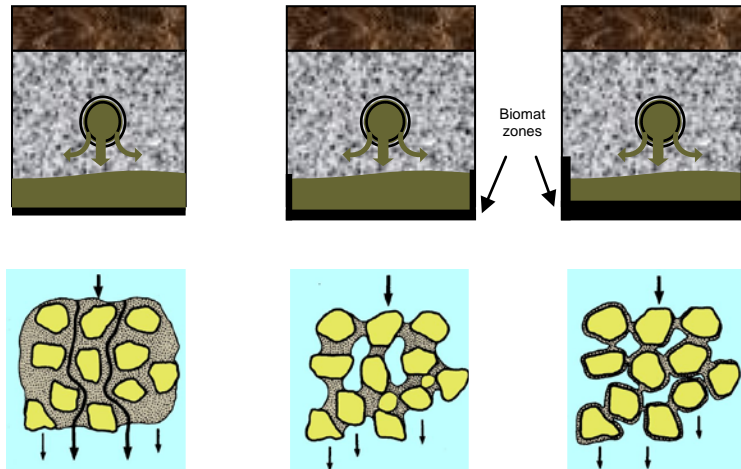
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Table 1. Septic tank effluent quality for key pollutants

Effluent Parameter	(Whelan and Titamnis 1982)	Beavers and Gardner (1993)	Gardner <i>et al.</i> (1997)	Charles <i>et al.</i> (2004) ^A
BOD ₅ (mg/L)	52 - 316	150 - 180	120 - 180	224
Suspended solids (mg/L)	22 - 47	100 - 180	40 - 190	379
Total N (mg/L)	74 - 237	50 - 60	40 - 50	160
Total P (mg/L)	12.3 - 26	10 - 15	10 - 15	21
Faecal coliforms (cfu/100mL)	-	10 ⁵ - 10 ⁷	10 ⁵ - 10 ⁷	10 ⁶ ^B

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A Mean

B Thermotolerant coliforms

Table 2 Summary of selected research investigating the removal of nutrients and pathogens in soil absorption systems

Reference	Summary of research	Removal efficiencies and comments
Nutrients (Walker <i>et al.</i> 1973a) (Starr and Sawhney 1980)	Five field SAS studied. Organic N retained in biomat zone. Monitored movement of N and C from SAS in a coarse sand.	All NH ₄ → NO ₃ within 2cm of biomat in unsaturated soil. Rainfall variability influenced NH ₄ / NO ₃ speciation. NH ₄ at depths >90cm in wet periods (anaerobic soil).
(Kristiansen 1981b) (Whelan and Barrow 1984a, 1984b) (Stewart and Reneau 1988)	Pilot sand filters tested N removal and biomat zone influence. Movement of effluent in 7 SAS investigated. Measured nutrients in GW ^A in sandy soil Fluctuating GW monitored near SAS in sandy loam.	Low N loss due to lack of labile C and anaerobic conditions. Organic N accumulated in biomat zone. NO ₃ mobile in GW. Poor P adsorption in sandy subsoil. >99% P removal. Denitrification observed during rising WT ^B .
(Cogger 1988)	Effects of STE loading rate and WT depth on treatment in sandy soil. Examined shallow and deep wells.	Saturated, anaerobic conditions ↑ NH ₄ in GW (30cm). Unsaturated conditions N removal high due to aerobic then anaerobic (GW) pathway of effluent - aiding denitrification.
(Pell and Nyberg 1989a, 1989b) (Gerritse <i>et al.</i> 1995a)	Measured nutrient and organic matter removal rates in newly operating sand filter and columns. GW monitoring near SAS in sandy soil. Bromide tracer used. One system studied.	83% P removal in ~75cm unsaturated sand. 91% COD ^C removal in 15cm unsaturated sand. Total nitrification in <15cm of unsaturated sand 80% of inorganic N from STE removed within 10m. Fluctuating WT promoted denitrification. P movement to GW slow.
(Geary 2004)	Instrumented SAS using piezometers and suction lysimeters to monitor GW. Tracer used to determine GW flow pathways. Soil columns with organic layers to ↑ N removal via denitrification	Found low N removal rates near SAS but substantial reduction 75 to 3.8mg/L of nitrate after flow through riparian strip. Average total N removal ↑ from 31% to 67% with organic layer present
Pathogens (Bedessem <i>et al.</i> 2005)	Major research effort including instrumentation of 19 SAS for hydraulic and purification monitoring in a range of soil types. Laboratory columns. Layered soils (representing mounds).	3-log reduction of pathogens within 38cm below trench. Largest reduction in biomat zone. Complete removal of FC ^D and FS ^E within 90cm of sand underlain by silt.
(Kristiansen 1981c) (Stewart and Reneau 1988)	Pilot sand filters tested bacterial removal and biomat zone influence. Fluctuating GW monitored near SAS in sandy loam.	2 to 4-log FC reduction. Clogging significant in FC removal. 5-log reduction in FC <10m distance and 1.5m depth to SAS
(Cogger 1988) (Alhajjar <i>et al.</i> 1988)	Effects of STE loading rate and WT depth on treatment in sandy soil. Down gradient GW monitored from 17 SAS. Newly developed biomat zone reported to be effective in filtering bacteria but not virus	5-log FC; 5-log FS ↓ in 60cm of unsaturated soil 4-log FC; 3-log FS ↓ in <1m depth, <6m distance of SAS. Poliovirus was not effectively removed.
(Postma <i>et al.</i> 1992)	GW monitoring from 3 seasonally-used SAS (gravelly fill material). Biomat zone not well developed in these systems. No 'control' (ie permanent SAS) used, so site factors cannot be discounted in results.	Estimated 4-log FC ↓ But 1.5m of unsaturated sand still high. Absence of proper biomat limited adequate removal. <i>Clostridium perfringens</i> poorly inactivated in unsaturated zone.
(Stevik <i>et al.</i> 1999) (van Cuyk <i>et al.</i> 2001b) (van Cuyk <i>et al.</i> 2004)	Column experiments investigating <i>E. coli</i> removal in filter media. 3-D lysimeter studies in medium sand. Field and laboratory studies of microbial purification in effluent.	Highest removal in upper column – dosing rate important. >90% removal of FC within 30cm of unsaturated sand. 2 to 3-log reduction in bacteriophages within 30-60cm unsaturated depth (field). Nearly complete removal FC.

^AGW - groundwater, ^BWT - water table, ^CCOD – chemical oxygen demand, ^DFC - faecal coliforms, ^EFS - faecal streptococci

Table 3 Summary of conclusions from various studies investigating contamination of waters from onsite systems

Reference	Summary of investigation	Hydraulic link to SAS established ^a	Reported SAS-related impacts ^b
Nutrients			
(Walker <i>et al.</i> 1973b)	Wisconsin, USA. GW sampling in loamy sand. Elevated nitrate (NO ₃ ⁻) levels in GW. NO ₃ ⁻ concentrations >10mg/L 30m down gradient from SAS	No tracers but NO ₃ ⁻ levels suggests a strong link. No control data.	No. Authors suggest that nitrate from SAS minor compared with other land uses.
(Jones and Lee 1979)	Wisconsin, USA. 4 yr GW monitoring. No evidence for PO ₄ movement from SAS in sandy soil. Nutrients in SW from GW low.	Yes. Used EC and chloride (Cl ⁻) data as indicator (tracer)	No. Authors suggest that SAS nutrients minor compared with other land uses
(Katz <i>et al.</i> 1980)	Compared GW NO ₃ ⁻ in sewered and non-sewered areas. No significant differences found in 25 yrs of data.	No, other land uses also contributing to nitrate loads throughout period of study	No. Authors suggest a range of land uses would have contributed to nitrate in GW
(Gilliom and Patmont 1983)	Puget Sound, USA. 23 monitoring wells downstream of 8 SAS adjacent to Lake Pine. Movement of >1% of STE P rare.	Yes, used Cl ⁻ to infer SAS link.	Nothing reported in study. Later studies have determined lake is eutrophic (Jacoby <i>et al.</i> 1997).
(Valiela <i>et al.</i> 1988)	Buttermilk Bay, USA. Calculated N, P loadings from SAS into bay and interception rates by denitrification etc	Water sampling and modelling suggests link.	Insufficient data to be certain, as high nutrient interception rates within catchment.
(Gibbs 1991)	Lake Taupo, New Zealand. GW monitoring in retro-sewered town. Possible storage of N in unsaturated zone, N processes not discussed.	No. Nutrient concentrations in GW declining since town sewered.	Later studies indicate agricultural land use to be severe WQ impact on lake (Edgar 1999).
(Robertson <i>et al.</i> 1991)	Ontario, Canada. GW monitoring of 2 SAS. NO ₃ ⁻ mobile in GW but good denitrification in enriched anaerobic sediments.	Yes, bromide (Br ⁻) tracers used.	Study did not indicate previous or existing eutrophication in region.
(Weiskel and Howes 1992)	Buttermilk Bay, USA. GW monitoring of nutrient movement from 2 SAS and 2 cesspools.	WQ monitoring suggests link. Inorganic N higher in GW than P	No. Authors suggest that P retention in ground water is effective and that SAS “contribute little to eutrophication”.
(Lapointe <i>et al.</i> 1990; Lapointe and Clark 1992)	Florida Keys, USA. 30 water sampling stations, twice/yr. High P and N attributed to OWTs. Sewage outfall located in area.	No. No tracers used. Specific SAS link undetermined.	Yes eutrophication studied in area. OWTs considered part of overall contribution but no estimated loads from non-sewered areas.
(Paul <i>et al.</i> 1995)	Florida Keys, USA. Tracers used to seed septic tanks and injection wells. Found tracers in septic tank moved to marine waters in <24 hrs. Tidal movement a factor.	Yes with use of tracers.	Yes eutrophication studied in area. OWTs considered part of overall contribution but no estimated loads from non-sewered areas.
(Gerriste <i>et al.</i> 1995b)	GW monitoring near SAS in sandy soil. High N reduction. Fluctuating WT promoted denitrification.	Yes, Br ⁻ tracer used.	Study did not indicate any reported impacts. Agricultural uses ↑ N in GW.
(Harman <i>et al.</i> 1996)	Ontario, Canada, GW monitoring below 1.6m vadose zone under SAS. High NO ₃ ⁻ . Slow PO ₄ release.	Yes, Br ⁻ tracers.	Study did not indicate previous or existing eutrophication in region.
(Dillon <i>et al.</i> 1999; Dillon <i>et al.</i> 2000)	Florida Keys, USA. Tracers in sewage injection well. Found rapid horizontal & vertical plume path. Dilution up to 7x by GW and SW.	No. Injection well plume was studied only. No soil-based systems studied.	Yes eutrophication studied in area. OWTs considered part of overall contribution but no estimated loads from non-sewered areas.
(Moore <i>et al.</i> 2003)	Seattle, USA. Compared eutrophication in lakes draining developed and undeveloped land. Non-sewered lakes had significantly higher P and chlorophyll- <i>a</i> than undeveloped lakes but less P than sewered lakes.	WQ monitoring suggests link.	Non-sewered lakes believed to be more eutrophic than sewered or undeveloped. No N measured.
(Steffy and Kilham 2004)	Penns., USA. δ ¹⁵ N stable-isotope analysis to detect sewage - derived N. Compared sewered and non-sewered areas.	Not directly though δ ¹⁵ N used as an indicator of anthropogenic N inputs	Non-sewered areas had elevated δ ¹⁵ N in food web compared with sewered areas.

Pathogens	Study	Findings	Conclusions
(Reneau and Petry 1975)	Virginia, USA. 3 SAS instrumented. Few FC observed at depth. Concluded GW not contaminated from vertical movement of FC.	Yes - monitoring above and below drainfield.	Study did not discuss / identify previous or existing waterborne-diseases in region.
(Reneau <i>et al.</i> 1975)	SW and GW bacteriological sampling. Variation in results. Surcharging observed in unsuitable soils.	No tracers but WQ monitoring suggests a strong link.	No. Area sewered during study.
(Rahe <i>et al.</i> 1978)	Oregon, USA. <i>E. coli</i> movement in simulated saturated conditions. Tracer injected into lines in soil trenches.	Unsure, operating SAS not studied only constructed soil 'trenches'.	N/A.
(Vaughn <i>et al.</i> 1983)	Long Island, USA. Viruses detected 67m and 18m depths from large septic tank-leaching pool system in sandy GW.	Unsure. Leaching 'pools' not soil-based absorption system used.	Unsure. Ongoing studies carried out on WQ in Long Island Sound.
(Alhajjar <i>et al.</i> 1988)	Wisconsin, USA. Down gradient GW monitored from 17 SAS. No tracer bacteria but poliovirus detected in GW	Yes, tracers (poliovirus and Cl ⁻) used	No although later studies in region have suggested illness links to contaminated wells (see Borchartd <i>et al</i> 2003 below)
(Postma <i>et al.</i> 1992)	Rhode Island, USA. GW monitored from 3 seasonally-used SAS. Poor FC and nutrient removal	Yes, NO ₃ ⁻ as tracer and WQ monitoring suggests a strong link.	Study did not identify previous or existing waterborne-diseases in region.
(Hoxley and Dudding 1994)	Victoria, Australia. GW monitoring in 2 non-sewered towns. NO ₃ ⁻ and <i>E. coli</i> reported in GW in Venus Bay. No data given.	No. GW monitoring suggests a possible link.	Study did not identify previous or existing waterborne-diseases in region.
(DeBorde <i>et al.</i> 1998)	Montana, USA. Instrumentation of school SAS and GW monitoring for viruses. Low levels detected only.	Yes Br ⁻ and coliphage tracers used.	Study did not identify previous or existing waterborne-diseases in region.
(Whitehead and Geary 2000)	Tasmania, Australia. GW monitoring non-sewered area. High nitrate concentrations measured in areas of residential clusters. FC almost undetectable at all sites.	Yes, NO ₃ ⁻ as tracer and WQ monitoring suggests a strongly link. Limited sample size.	Study did not identify previous or existing waterborne-diseases in region.
(Frenzel and Couvillion 2002)	Alaska, USA. SW samples from areas of varying development density. Sewered areas had significantly higher faecal-indicator bacteria than non-sewered areas	No. SW data compared for different catchment land uses. Storm sewers linked to high faecal-indicator bacteria.	Study did not identify previous or existing waterborne-diseases in region.
(Bopp <i>et al.</i> 2003)	New York, USA. Investigation of largest reported outbreak of waterborne <i>E. coli</i> . GW supply located near school SAS. <i>E.coli</i> source may be animal origin.	Yes, dye seepage tests used and link detected in one well.	Yes. Largest reported outbreak of waterborne <i>E. coli</i> in USA. Direct cause by SAS not fully determined but likely.
(Borchartd <i>et al.</i> 2003)	Wisconsin, USA. Assessed association between septic system density and illness in children. Viral diarrhoea associated mainly with holding tanks not SAS	Unknown. Well water quality not actually tested in non-sewered areas that were studied.	Unknown, although authors suggest 11% of unexplained acute illness caused by ingesting faecal - contaminated well water
(Carroll <i>et al.</i> 2004)	Brisbane, Australia. GW and SW monitoring in high density non-sewered area. Elevated NO ₃ ⁻ and FC. Agricultural practices may contribute to NO ₃ ⁻ .	No. Found increase in nutrient concentrations in GW directly below township.	Study did not identify previous or existing waterborne-diseases in region. GW not a drinking water source.

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^A A hydraulic link / pathway / connection has been established between the onsite system investigated and contaminant(s) investigated in receiving ground / surface waters.

^B Environmental and / or public health impact associated with wastewater contaminants reported in the area of investigation.

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Table 4. Summary of some reported minimum sustainable lot sizes and OWTS densities

Lot size (m ²)	System density (per km ²)	Comments	Reference
65,000	15	Septic system density considered potential for ground water contamination	(USEPA 1977)
2000 – 4000	500 - 250	Simple modelling showed increased N concentration below SAS as lot size decreased	(Perkins 1984)
1000 – 12,000	1000 - 85	Range of densities where ground water contamination had been reported	(Yates 1985)
10,000	100	Example density for NSW coastal town based on minimum assimilative buffer area for pollutants (N, P, pathogens)	(Jelliffe 1999)
2000 - 4000	500 - 250	Based on average nutrient and hydraulic loadings from OWTS and minimum setback distances for pathogens	(Geary and Gardner 1998)
50,000 – 100,000	10-20	Recommended in environmentally sensitive areas based on N and P assimilation	(Gerritse 2002)

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Table 5. Summary of some key areas of further OWTS research

Site-scale	Catchment-scale
Effects of pressure dosing on LTAR for in Australian soils	Risk-based decision models e.g further validation of OSRAS, DAM
Oxygen dynamics under biomat zone	Quantifying contaminant loads from on-site systems
Denitrification in SAS and technologies for removal of N	Sustainable on-site system densities and separation distances
Treatment capacities of a greater range of soil types in Australia, e.g . colder climates	Monitoring sewered v non-sewered catchments – looking for the “smoking gun”
Effects of pre-treated effluent and innovative soil-based designs	Role of riparian zone and fluctuating water tables in nitrate removal and P sorption in sediments
Predicting biomat zone development and its role in long term effluent treatment / hydraulics	Use of tracers to identify contaminant pathways in surface and groundwaters

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1187 **Fig. 1.** Schematic representation of system layout and main processes (a); plan and cross section view
1188 of the trenches in a soil absorption system (b & c).

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1190 **Fig. 2** A commonly observed schematic pattern of wastewater infiltration rate decline through soil
1191 infiltrative surface over time, adapted from Otis (1984).

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1193 **Fig. 3.** Definition diagram of Equation 2. θ_u is the volumetric water content of the underlying soil
1194 (cm^3/cm^3), θ_s is the saturated volumetric water content of the underlying soil (cm^3/cm^3), z is soil depth
1195 (cm), and Ψ_u is the soil moisture potential of the underlying soil

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1197 **Fig. 4.** Predicted effect of increasing R_b on steady-state flow rates for a range of Australian soils (Beal
1198 et al. 2004a) (Note: X axis not to scale)

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1200 **Fig. 5.** Cross section of trench with increasingly resistant biomat zone (top) resulting in increasingly
1201 unsaturated flow (below).

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